# Molecular dynamics in different ensembles

### **Javier Junquera**



### **Equations of motion for atomic systems**

Classical equation of motion for a system of N molecules interacting via a potential  ${\cal V}$ 

#### The most fundamental form: the Lagrangian equation of motion

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}_k} \right) - \left( \frac{\partial \mathcal{L}}{\partial q_k} \right) = 0$$

Where the Lagrangian function  $\mathcal{L}(\vec{q}, \dot{\vec{q}})$  is defined in terms of the kinetic and potential energies, and is considered to be a function of the generalized coordinates  $q_k$  and their time derivatives  $\dot{q}_k$ 

$$\mathcal{L} = \mathcal{K} - \mathcal{V}$$

## Equations of motion for atomic systems in cartesian coordinates

Classical equation of motion for a system of N molecules interacting via a potential  ${\cal V}$ 

If we consider a system of atoms with Cartesian coordinates  $\vec{r_i}$ , and the usual definitions of the kinetic and potential energies

$$\mathcal{K} = \sum_{i=1}^{N} \sum_{\alpha} \frac{p_{i\alpha}^2}{2m_i}$$

 $\mathcal{V} = \sum_{i} v_1(\vec{r_i}) + \sum_{i} \sum_{j>i} v_2(\vec{r_i}, \vec{r_j}) + \sum_{i} \sum_{j>i} \sum_{k>j>i} v_3(\vec{r_i}, \vec{r_j}, \vec{r_k}) + \dots$ 

Then, the equation of motion transforms into

$$m_i \frac{d^2 \vec{r_i}}{dt^2} = \vec{f_i}$$

where  $m_i$  is the mass of atom i and the force on that atom is given by

 $ec{f_i} = 
abla_{ec{r_i}} \mathcal{L} = abla_{ec{r_i}} \mathcal{V}$ 

# Equations of motion for atomic systems in cartesian coordinates

Classical equation of motion for a system of N molecules interacting via a potential  ${\cal V}$ 

$$m_i \frac{d^2 \vec{r_i}}{dt^2} = \vec{f_i}$$

This equation also aplies to the center of mass motion of a molecule, with the force begin the total external force acting on it

# Hamilton's equation of motion in cartesian coordinates

$$\dot{\vec{r}_i} = \frac{\vec{p_i}}{m_i}$$

For a derivation of these expressions, read Goldstein, Chapter 8

$$\dot{\vec{p}_i} = -\nabla_{\vec{r}_i} \mathcal{V} = \vec{f_i}$$

### Hamilton or Lagrange equations of motion

Lagrange's equation

Hamilton's equations



$$\dot{ec{p}_i} = -
abla_{ec{r}_i} \mathcal{V} = ec{f_i}$$

To compute the center of mass trajectories involves solving...

A system of 3*N* second order differential equations

Or an equivalent set of 6*N* first-order differential equations

$$m_i \ddot{\vec{r}_i} = \vec{f_i}$$

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$$m_i \ddot{\vec{r}_i} = \vec{f_i}$$

### **Conservation laws**

Assuming that  $\,\mathcal{K}\,$  and  $\,\mathcal{V}\,$  do not depend explicitly on time, so that

$$\frac{\partial \mathcal{H}}{\partial t} = 0$$

Essential condition: No explicitly time dependent or velocity dependent force acting

Then, the total derivative of the Hamiltonian with respect to time

$$\dot{\mathcal{H}} = \frac{d\mathcal{H}}{dt} = \frac{\partial\mathcal{H}}{\partial t} + \frac{\partial\mathcal{H}}{\partial\vec{p}}\frac{\partial\vec{p}}{\partial t} + \frac{\partial\mathcal{H}}{\partial\vec{q}}\frac{\partial\vec{q}}{\partial t}$$

#### From the Hamilton's equation of motion

$$\dot{q}_{k} = \frac{\partial \mathcal{H}}{\partial p_{k}} \qquad \dot{p}_{k} = -\frac{\partial \mathcal{H}}{\partial q_{k}}$$
$$\dot{\mathcal{H}} = \frac{\partial \mathcal{H}}{\partial t} = \frac{\partial \mathcal{H}}{\partial t} - \frac{\partial \mathcal{H}}{\partial \vec{p}} \frac{\partial \mathcal{H}}{\partial \vec{q}} + \frac{\partial \mathcal{H}}{\partial \vec{q}} \frac{\partial \mathcal{H}}{\partial \vec{p}} = 0$$

The Hamiltonian is a constant of motion

Independent of the existence of an external potential

### The equations are time reversible

By changing the signs of all the velocities and momenta, we will cause the molecules to retrace their trajectories.

If the equations of motion are solved correctly, the computer-generated trajectories will also have this property

Standard method to solve ordinary differential equations: the finite difference approach

We attempt to obtain the position, velocities, etc. at a later time  $t+\delta t$  , to a sufficient degree of accuracy

Notes:

The equations are solved on a step by step basis

The choice of the time interval  $\delta t$  will depend on the method of solution, but  $\delta t$  will be significantly smaller than the typical time taken for a molecule to travel its own length

# Many different algorithms within the finite different methodology

**Predictor-corrector algorithm** 

# If the classical trajectory is continuous, then an estimate of the positions, velocities, accelerations at $t + \delta t$ can be obtained by a Taylor expansion about time t

$$\vec{r}^{p}(t+\delta t) = \vec{r}(t) + \vec{v}(t)\delta t + \frac{1}{2}\vec{a}(t)\delta t^{2} + \frac{1}{6}\vec{b}(t)\delta t^{3} + \cdots$$
$$\vec{v}^{p}(t+\delta t) = \vec{v}(t) + \vec{a}(t)\delta t + \frac{1}{2}\vec{b}(t)\delta t^{2} + \cdots$$
$$\vec{a}^{p}(t+\delta t) = \vec{a}(t) + \vec{b}(t)\delta t + \cdots$$
$$\vec{b}^{p}(t+\delta t) = \vec{b}(t) + \cdots$$
$$p \text{ stands for "predicted"}$$

 $\vec{r}$  stands for the complete set of positions

- $ec{v}$  stands for the complete set of velocities
- $\vec{a}$  stands for the complete set of accelerations
- $\vec{b}$  stands for the complete set of third derivatives of the position

We store four "vectors" per atom:  $\vec{r}, \vec{v}, \vec{a}$ , and  $\vec{b}$ 

If the classical trajectory is continuous, then an estimate of the positions, velocities, accelerations at  $t + \delta t$  can be obtained by a Taylor expansion about time t

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$$\vec{a}^{p}(t+\delta t) = \vec{a}(t) + \vec{b}(t)\delta t + \cdots$$
$$\vec{b}^{p}(t+\delta t) = \vec{b}(t) + \cdots$$
$$p \text{ stands for "predicted"}$$

If we truncate the expansion retaining the terms given above

We have achieved our goal of approximately advancing the values of the dynamical quantites from one time step to the next We will not generate correct trajectories as time advances because we have not introduced the equations of motion

# The equations of motion are introduced through the correction step

From the new predicted positions  $\vec{r}^p(t + \delta t)$  we can compute the forces at time  $t + \delta t$ , and hence correct accelerations  $\vec{a}^c(t + \delta t)$ 

The correct accelerations can be compared with the predicted accelerations to estimate the size of the error in the prediction step

 $\Delta \vec{a}(t+\delta t) = \vec{a}^c(t+\delta t) - \vec{a}^p(t+\delta t)$ 

This errors, and the results of the predictor step, are fed into the corrector step

$$\vec{r}^{c}(t+\delta t) = \vec{r}^{p}(t+\delta t) + c_{0}\Delta\vec{a}(t+\delta t)$$
$$\vec{v}^{c}(t+\delta t) = \vec{v}^{p}(t+\delta t) + c_{1}\Delta\vec{a}(t+\delta t)$$
$$\vec{a}^{c}(t+\delta t) = \vec{a}^{p}(t+\delta t) + c_{2}\Delta\vec{a}(t+\delta t)$$
$$\vec{b}^{c}(t+\delta t) = \vec{b}^{p}(t+\delta t) + c_{3}\Delta\vec{a}(t+\delta t)$$

These positions, velocities, etc. are better approximations to the true positions, velocities, etc.

# "Best choices" (leading to optimum stability and accuracy of the trajectories) for the coefficients $c_0, c_1, c_2$ and $c_3$ discussed by Gear

Different values of the coefficients are required if we include more (or fewer) position derivatives in our scheme

The coefficients also depend upon the order of the differential equation being solved (second order in our case)

Table E.1 Gear corrector coefficients for a first-order equation						
Values	c <sub>o</sub>	<i>c</i> <sub>1</sub>	<i>c</i> <sub>2</sub>	c <sub>3</sub>	C4	C <sub>5</sub>
3	5/12	1	1/2			
4	3/8	1	3/4	1/6		
5	251/720	1	11/12	1/3	1/24	
6	95/288	1	25/24	35/72	5/48	1/120

Table E.2 Gear corrector coefficients for a second-order equation

Values	$c_0$	<i>c</i> <sub>1</sub>	<i>c</i> <sub>2</sub>	<i>c</i> <sub>3</sub>	C4	<i>c</i> <sub>5</sub>
3	0	1	1			
4	1/6	5/6	1	1/3		
5	19/120	3/4	1	1/2	1/12	
6	3/20	251/360	1	11/18	1/6	1/60

If the positions, velocities, accelerations, etc. are unscaled, factors involving the time scaled are required (see algorithm below)

### Implementation of Gear's predictor-corrector algorithm

SUBROUTINE PREDIC ( DT )

The predictor part

С	***************************************
С	** PREDICTOR ROUTINE **
С	** **
С	** IN TIMESTEP-SCALED VARIABLES THE PREDICTOR IS THE PASCAL **
С	** TRIANGLE MATRIX. IN UNSCALED VARIABLES IT IS A TAYLOR SERIES **
С	** **
С	** USAGE: **
С	** **
С	** PREDIC IS CALLED TO ADVANCE THE COORDINATES, VELOCITIES ETC. **
С	** BY ONE TIMESTEP DT, PRIOR TO FORCE EVALUATION. **
С	*****
	INTEGER N
	PARAMETER ( $N = 108$ )
	REAL DT
	REAL RX(N), RY(N), RZ(N)
	REAL VX(N), VY(N), VZ(N)
	REAL AX(N), AY(N), AZ(N)
	REAL BX(N), BY(N), BZ(N)
	REAL CX(N), CY(N), CZ(N)
	REAL FX(N), FY(N), FZ(N)
	INTEGER I
	REAL C1, C2, C3, C4
С	***************************************
!	Compute the coefficients for the Taylor expansion
	C1 = DT
	C2 = C1 * DT / 2.0
	C3 = C2 * D1 / 3.0
	C4 = C3 * D1 / 4.0
:	DO 100 T - 1 N
	Predict the new positions
	A Taylor expansion up to fourth order is done
i	That means that we have to store upto five arrays per atom
	RX(I) = RX(I) + C1*VX(I) + C2*AX(I) + C3*RX(I) + C4*CX(I)
	RY(I) = RY(I) + C1*VY(I) + C2*AY(I) + C3*BY(I) + C4*CY(I)
	RZ(I) = RZ(I) + C1*VZ(I) + C2*AZ(I) + C3*BZ(I) + C4*CZ(I)
!	Predict the new velocities
	VX(I) = VX(I) + C1*AX(I) + C2*BX(I) + C3*CX(I)
	VY(I) = VY(I) + C1*AY(I) + C2*BY(I) + C3*CY(I)
	VZ(I) = VZ(I) + C1*AZ(I) + C2*BZ(I) + C3*CZ(I)
!	Predict the new accelerations
	AX(I) = AX(I) + C1*BX(I) + C2*CX(I)
	AY(I) = AY(I) + C1*BY(I) + C2*CY(I)
	AZ(I) = AZ(I) + C1*BZ(I) + C2*CZ(I)
!	Predict the new third derivatives of the positions
	BX(I) = BX(I) + C1 * CX(I)
	BY(I) = BY(I) + C1*CY(I)
	BZ(I) = BZ(I) + C1*CZ(I)
100	ENDDO
	RETURN
	END

#### Implementation of Gear's predictor-corrector algorithm

!

100

SU	JBRUUTINE CURREC ( DT, M, K )	
***	***************************************	**
**	CORRECTOR ROUTINE	**
**		**
**	CORRECTS POSITIONS, VELOCITIES ETC. AFTER FORCE EVALUATION.	**
**	TN TIMESTED-SCALED VARIABLES THE NUMERICAL COFFETCIENTS ARE	**
<b>π</b> π	CIVEN BY GEAD (DEE ADOUE), 10/100 2/4 1 1/0 1/10	тт 
**	GIVEN BY GEAR (REF ABUVE): 19/120, 3/4, 1, 1/2, 1/12.	**
**	IN UNSCALED FORM THESE MUST BE MULTIPLIED BY FACTORS	**
**	INVOLVING THE TIMESTEP AS SHOWN HERE.	**
**		**
**	PRINCIPAL VARIABLES:	**
**		**
ተተ	REAL M AIUMIC MASS	**
**	REAL K KINETIC ENERGY PER ATUM	**
**	REAL GEARO, GEAR1, GEAR2, GEAR3 GEAR COEFFICIENTS	**
**		**
**	USAGE:	**
**		**
**	TT IS ASSUMED THAT INTERMOLECULAR FORCES HAVE BEEN CALCULATED	**
**	AND GTODED IN EX EX EZ GODDEG GINDLY ADDITEG THE GODDEGTOD	**
**	AND STURED IN FX, FY, FZ. CURREC SIMPLY APPLIES THE CURRECTUR	**
**	EQUATIONS BASED ON THE DIFFERENCES BETWEEN PREDICTED AND	**
**	EVALUATED ACCELERATIONS. IT ALSO CALCULATES KINETIC ENERGY.	**
***	***********	**
	INTEGER N	
	PARAMETER (N = 108)	
	REAL DI	
	REAL $RX(N)$ , $RY(N)$ , $RZ(N)$	
	REAL $VX(N)$ , $VY(N)$ , $VZ(N)$	
	REAL $AX(N)$ , $AY(N)$ , $AZ(N)$	
	REAL $BX(N)$ , $BY(N)$ , $BZ(N)$	
	REAL $CX(N) CY(N) CZ(N)$	
	$\begin{array}{ccc} \mathbf{PEAI} & \mathbf{EV}(\mathbf{N}) & \mathbf{EV}(\mathbf{N}) & \mathbf{ET}(\mathbf{N}) \\ \mathbf{EV}(\mathbf{N}) & \mathbf{EV}(\mathbf{N}) & \mathbf{ET}(\mathbf{N}) \\ \end{array}$	
	$\mathbf{R} = \mathbf{R} \mathbf{R} \mathbf{R} \mathbf{R} \mathbf{R} \mathbf{R} \mathbf{R} \mathbf{R}$	
	REAL M, K	
	INTEGER I	
	REAL AXI, AYI, AZI	
	REAL CORRX, CORRY, CORRZ	
	REAL C1. C2. C3. C4	
	REAL CR CV CB CC	
	DEAL CEADO CEADO CEADO CEADO	
	REAL GEARD, GEARI, GEARD, GEART	
	PARAMETER ( GEARO = 19.0 / 120.0, GEAR1 = 3.0 / 4.0,	
:	GEAR3 = 1.0 / 2.0, GEAR4 = 1.0 / 12.0 )	
***	***************************************	**
	C1 = DT	
	C2 = C1 * DT / 2.0	
	$C_3 = C_2 * DT / 3.0$	
	CA = C2 + DT / A O	
	C4 = C3 * D1 / 4.0	
	CR = GEARO * C2	
	CV = GEAR1 * C2 / C1	
	CB = GEAR3 * C2 / C3	
	CC = GEAR4 * C2 / C4	

K = 0.0Loop over all the atoms in the system DO 100 I = 1, N Compute the correct accelerations AXI = FX(I) / MAYI = FY(I) / MAZI = FZ(I) / MCompare with the predicted accelerations to estimate the size of the errors CORRX = AXI - AX(I)CORRY = AYI - AY(I)CORRZ = AZI - AZ(I)Correct the positions. RX(I) = RX(I) + CR \* CORRXRY(I) = RY(I) + CR \* CORRYRZ(I) = RZ(I) + CR \* CORRZCorrect the velocities. VX(I) = VX(I) + CV \* CORRXVY(I) = VY(I) + CV \* CORRYVZ(I) = VZ(I) + CV \* CORRZCorrect the accelerations. AX(I) = AXIAY(I) = AYIAZ(I) = AZICorrect the third derivative of the positions. BX(I) = BX(I) + CB \* CORRXBY(I) = BY(I) + CB \* CORRYBZ(I) = BZ(I) + CB \* CORRZCorrect the fourth derivative of the positions. CX(I) = CX(I) + CC \* CORRXCY(I) = CY(I) + CC \* CORRYCZ(I) = CZ(I) + CC \* CORRZCompute the corrected kinetic energy K = K + VX(I) \*\* 2 + VY(I) \*\* 2 + VZ(I) \*\* 2ENDDO K = 0.5 \* M \* KRETURN END

#### The corrector part

### The corrector step might be iterated till convergence

New correct accelerations are computed from the positions  $\vec{r}^c$  and compared with the current values of  $\vec{a}^c$ , so as to further refine the positions, velocities, etc.

### In many applications this iteration is key to obtaining an accurate solution

However, each iteration requires a computation of the forces from particle positions (the most time-consuming part of the simulation) ⇒ A large number of corrector iterations would be very expensive. Normally one (occasionally two) corrector steps are carried out

### General step of a stepwise Molecular Dynamics simulation



### **Desirable qualities for a successful simulation algorithm**

It should be fast and require little memory

Since the most time consuming part is the evaluation of the force, the raw speed of the integration algorithm is not so important

It should permit the use of long time step  $\,\delta t$ 

Far more important to employ a long time step. In this way, a given period of simulation time can be covered in a modest number of steps

It should duplicate the classical trajectory as closely as possible

It should satisfy the known conservation laws for energy and momentum, and be time reversible

It should be simple in form and easy to program

Involve the storage of only a few coordinates, velocitites,...

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It should be simple in form and easy to program

Involve the storage of only a few coordinates, velocitites,...

The accuracy and stability of a simulation algorithm may be tested comparing the result with analytical simple models (Harmonic oscillator, for instance)

Any approximate method of solution will dutifully follow the classical trajectory indefinetely

Small differences in the initial conditions

**Small numerical errors** 

Any two trajectories which are initially very close will eventually diverge from one another exponentially with time Any small perturbation, even the tiny error associated with finite precision arithmetic, will tend to cause a computer-generated trajectory to diverge from the true classical trajectory with which it is initially coincident

### The accuracy and stability of a simulation algorithm may be tested comparing the result with analytical simple models (Harmonic oscillator, for instance)

Any approximate method of solution will dutifully follow the classical trajectory indefinetely

#### **Divergence of trajectories in** molecular dynamics

As the time proceeds, other mechanical

quantites become statistically uncorrelated Molecules **Small differences in the** (a) perturbed from the (b)  $10^{2}$  r 0.4% 10-3 initial positions at initial conditions time steps t=0 bv  $\Delta X / X$ time steps  $10^{0}$ 1000 500 500 10<sup>-3</sup> -0.4%10-2 0.4% 10-6 10<sup>-6</sup>  $10^{-3}\sigma$ Any two trajectories which are **1**10<sup>-9</sup> DX /X time steps initially very close will ⊿r 10<sup>-4</sup> 1000 \$500 eventually diverge from one -0.4%  $10^{-6}\sigma$ 10 0.4% another exponentially with time time steps 10 500  $10^{-9}\sigma$ -0.4%L 10<sup>-10</sup>  $\vec{r}_i^{0}(t)$  Reference simulation  $|\Delta \vec{r}|^2 = \frac{1}{N} \sum_{i=1}^{N} |\vec{r_i}(t) - \vec{r_i}^0(t)|^2$ 

 $\vec{r}_i(t)$  Perturbed simulation

### The accuracy and stability of a simulation algorithm may be tested comparing the result with analytical simple models (Harmonic oscillator, for instance)

Any approximate method of solution will dutifully follow the classical trajectory indefinetely

No integration algorithm will provide an essentially exact solution for a very long time

But this is not really required... What we need are:

Exact solutions of the equations of motion for times comparable with the correlation times of interest, so we can calculate time correlation functions The method has to generate states sampled from the microcanonical ensemble. The emphasis has to be given to the energy conservation.

The particles trajectories must stay on the appropriate constant-energy hypersurfaces in phase space to generate correct ensemble averages

### Energy conservation is degraded as time step is increased

All simulations involve a trade-off between



A good algorithm permits a large time step to be used while preserving acceptable energy conservation

### Parameters that determine the size of $\delta t$

- Shape of the potential energy curves
- Typical particle velocities

Shorter time steps are used at high-temperatures, for light molecules, and for rapidly varying potential functions

# The Verlet algorithm method of integrating the equations of motion: description of the algorithm

**Direct solution of the second-order equations** 

Method based on:

- the positions  $ec{r}(t)$
- the accelerations  $\vec{a}(t)$

- the positions from the previous step  $\vec{r}(t-\delta t)$ 

A Taylor expansion of the positions around *t* 

$$\vec{r}(t+\delta t) = \vec{r}(t) + \vec{v}(t)\delta t + \frac{1}{2}\vec{a}(t)\delta t^2 + \cdots$$
$$\vec{r}(t-\delta t) = \vec{r}(t) - \vec{v}(t)\delta t + \frac{1}{2}\vec{a}(t)\delta t^2 - \cdots$$

Adding the two equations  $\vec{r}(t + \delta t) + \vec{r}(t - \delta t) = 2\vec{r}(t) + \vec{a}(t)\delta t^{2} + \mathcal{O}(\delta t^{4})$   $\vec{r}(t + \delta t) = 2\vec{r}(t) - \vec{r}(t - \delta t) + \vec{a}(t)\delta t^{2} + \mathcal{O}(\delta t^{4})$ 

 $\vec{r}(t+\delta t) = 2\vec{r}(t) - \vec{r}(t-\delta t) + \vec{a}(t)\delta t^2 + \mathcal{O}(\delta t^4)$ 

#### **Remark 1**

The velocities are not needed to compute the trajectories, but they are useful for estimating the kinetic energy (and the total energy).

They can be computed a posteriori using [ $\vec{v}(t)$  can only be computed once  $\vec{r}(t + \delta t)$  is known]

$$\vec{v}(t) = \frac{\vec{r}(t+\delta t) - \vec{r}(t-\delta t)}{2\delta t} + \mathcal{O}(\delta t^2)$$

#### Remark 2

Whereas the errors to compute the positions are of the order of  $\delta t^4$  . The velocities are subject to errors of the order of  $\delta t^2$ 

$$\vec{r}(t+\delta t) = 2\vec{r}(t) - \vec{r}(t-\delta t) + \vec{a}(t)\delta t^2 + \mathcal{O}(\delta t^4)$$

#### **Remark 3**

The Verlet algorithm is properly centered:  $\vec{r}(t - \delta t)$  and  $\vec{r}(t + \delta t)$  play symmetrical roles.

The Verlet algorithm is time reversible

#### **Remark 4**

The advancement of positions takes place all in one go, rather than in two stages as in the predictor-corrector algorithm.

- Let us assume that we have available current (RX) and old (RXOLD).
- The current accelerations (AX) are evaluated in the force loop as usual.

100

Then, the coordinates are advanced in the following way

$$\vec{r}(t+\delta t) = 2\vec{r}(t) - \vec{r}(t-\delta t) + \vec{a}(t)\delta t^2 + \mathcal{O}(\delta t^4)$$

$$\vec{v}(t) = \frac{\vec{r}(t+\delta t) - \vec{r}(t-\delta t)}{2\delta t} + \mathcal{O}(\delta t^2)$$

SUMVSQ = 0.0 SUMVX = 0.0 SUMVY = 0.0 SUMVZ = 0.0
DO 100 I = 1, N
$\begin{array}{llllllllllllllllllllllllllllllllllll$
CONTINUE

- Let us assume that we have available current (RX) and old (RXOLD).
- The current accelerations (AX) are evaluated in the force loop as usual.

100

Then, the coordinates are advanced in the following way

Use of temporary variables (**RXNEWI**) to store the new positions.

This is necessary because the current values must be transferred to the "old" positions before being overwritten with the new variables.

The calculation of kinetic energy (SUMVSQ) and the total linear momentum (SUMVX) is included in the loop, since this is the only moment at which  $\vec{r}(t - \delta t)$  and  $\vec{r}(t + \delta t)$  are known.

SUMVSQ = 0.0 SUMVX = 0.0 SUMVY = 0.0 SUMVZ = 0.0	•
DO 100 I = 1,	Ν
RXNEWI = RYNEWI = RZNEWI = VXI = VXI = VZI = SUMVSQ = SUMVX = SUMVX = SUMVY = RXOLD(I) = RYOLD(I) = RX(I) = RX(I) = RZ(I) =	2.0 * RX(I) - RXOLD(I) + DTSQ * AX(I) 2.0 * RY(I) - RYOLD(I) + DTSQ * AY(I) 2.0 * RZ(I) - RZOLD(I) + DTSQ * AZ(I) ( RXNEWI - RXOLD(I) ) / DT2 ( RYNEWI - RYOLD(I) ) / DT2 ( RZNEWI - RZOLD(I) ) / DT2 SUMVSQ + VXI ** 2 + VYI ** 2 + VZI ** 2 SUMVX + VXI SUMVY + VYI SUMVZ + VZI RX(I) RY(I) RZ(I) RXNEWI RZNEWI
CONTINUE	



Known the positions at *t*, we compute the forces (and therefore the accelerations at *t*)

> Then, we apply the Verlet algorithm equations to compute the new positions

> > ...and we repeat the process computing the forces (and therefore the accelerations at  $t + \delta t$  )

# The Verlet algorithm method of integrating the equations of motion: advantages

The Verlet algorithm requires 9*N* words of storage (**RX**, **RXOLD**, **AX**, and the corresponding for the *y* and *z* coordinates)

The algorithm is exactly reversible in time, and, given conservative forces, is guaranteed to conserve linear momentum and energy

The method has been shown to have excellent energy conserving properties even in long time steps

The handling of velocities is rather awkward

It may introduce some numerical imprecision

$$\vec{r}(t+\delta t) = 2\vec{r}(t) - \vec{r}(t-\delta t) + \vec{a}(t)\delta t^2 + \mathcal{O}(\delta t^4)$$

A small term of order  $\mathcal{O}(\delta t^2)$  ...

…is added to a difference of large terms, of order  $~{\cal O}(\delta t^0)$ 

# The half-step "leap-frog" scheme tackles the deficiencies of the Verlet algorithm

#### Method based on:

- the positions $\vec{r}(t)$ - the accelerations $\vec{a}(t)$ - the mid-step velocities $\vec{v}(t - \delta t/2)$ 

#### Algorithm

 $\vec{r}(t+\delta t) = \vec{r}(t) + \vec{v}(t+\delta t/2)\delta t$ 

 $\vec{v}(t+\delta t/2) = \vec{v}(t-\delta t/2) + \vec{a}(t)\delta t$ 

### Scheme of the half-step "leap-frog" algorithm



The velocity equation is implemented first, and the velocities leap over the coordinates

 $\vec{v}(t+\delta t/2) = \vec{v}(t-\delta t/2) + \vec{a}(t)\delta t$ 

Then, we apply the leap-frog algorithm to compute the new positions  $\vec{r}(t + \delta t) = \vec{r}(t) + \vec{v}(t + \delta t/2)\delta t$ 

Known the new positions, we compute the forces and therefore the accelerations...

...and we repeat the process computing the new velocities at  $t+\delta t$ 

At a given *t*, we can compute the velocities, required to calculate the total energy

 $\vec{v}(t) = \frac{1}{2} \left[ \vec{v}(t + \delta t/2) + \vec{v}(t - \delta t/2) \right]$ 

# The half-step "leap-frog" scheme: advantages and disadvantages

#### **Advantages**

Elimination of velocities from the leap-frog equations, the method is algebraically equivalent to Verlet's algorithm

At no stage do we take the difference of two large quantities to obtain a small value, minimizing loss of precision on a computer

**Disadvantages** 

Still do not handle the velocities in a complete satisfactory way

# The velocity Verlet algorithm: algorithm and advantages

**Algorithm** 

$$\vec{r}(t+\delta t) = \vec{r}(t) + \vec{v}(t)\delta t + \frac{1}{2}\vec{a}(t)\delta t^2$$
$$\vec{v}(t+\delta t) = \vec{v}(t) + \frac{1}{2}\left[\vec{a}(t) + \vec{a}(t+\delta t)\right]\delta t$$

#### **Advantages**

Stores the positions, velocities, and accelerations at the same time t

**Minimizes rounds-off errors** 

The Verlet algorithm can be recovered by eliminating the velocities

### Scheme of the velocity Verlet algorithm



Known the positions, velocities and accelerations at *t*, we compute the new positions at  $t + \delta t$ 

At this point the kinetic energy is available

The velocities at mid step are computed using  $\vec{v}(t + \delta t/2) = \vec{v}(t) + \frac{1}{2}\vec{a}(t)\delta t$  The potential energy has been evaluated in the force loop

Known the new positions, we compute the forces and therefore the accelerations at

time  $t + \delta t$ 

The velocity move is completed

 $\vec{v}(t+\delta t) = \vec{v}(t+\delta t/2) + \frac{1}{2}\vec{a}(t+\delta t)\delta t$ 

### The velocity Verlet algorithm: advantages

The method uses 9*N* words of storage

Numerically stable

Very simple

### The velocity Verlet algorithm:

SUBROUTINE MOVEA ( DT, M )

COMMON / BLOCK1 / RX, RY, RZ, VX, VY, VZ, FX, FY, FZ

С	***************************************	**
С	** FIRST PART OF VELOCITY VERLET ALGORITHM *	**
С	**	**
C	** USAGE: *	**
C		**
C C	** THE FIRST PART OF THE ALGORITHM IS A TAYLOR SERIES WHICH	**
C	** ADVANCES FUSITIONS FROM I TO I + DI AND VELOCITES FROM ** T TO T + $DT/2$ AFTER THIS THE FORCE ROUTINE IS CALLED	**
C	**************************************	**
Ū		
	INTEGER N	
	PARAMETER ( $N = 108$ )	
	REAL DT, M	
	$\begin{array}{ccc} REAL & RX(N), RY(N), RZ(N) \\ \end{array}$	
	$\begin{array}{ccc} \text{REAL} & \text{VX}(N), & \text{VY}(N), & \text{VZ}(N) \\ \end{array}$	
	REAL $FX(N)$ , $FY(N)$ , $FZ(N)$	
	TNTEGER T	
	REAL DT2. DTSQ2	
С	***************************************	**
	DT2 = DT / 2.0	
	DISU2 = DI * DI2	
	DO 100 T = 1 N	
!	The new positions at time (t + delta t) are calculated	
-	RX(I) = RX(I) + DT * VX(I) + DTSO2 * FX(I) / M	
	RY(I) = RY(I) + DT * VY(I) + DTSQ2 * FY(I) / M	
	RZ(I) = RZ(I) + DT * VZ(I) + DTSQ2 * FZ(I) / M	
!	The velocities at mid-step are computed	
	VX(I) = VX(I) + DT2 * FX(I) / M	
	VY(I) = VY(I) + DT2 * FY(I) / M	
	VZ(I) = VZ(I) + DT2 * FZ(I) / M	
100		
100	חתמיז	
	RETURN	

END

### The velocity Verlet algorithm:

SUBROUTINE MOVEB ( DT, M, K )

COMMON / BLOCK1 / RX, RY, RZ, VX, VY, VZ, FX, FY, FZ

С	***************************************
С	** SECOND PART OF VELOCITY VERLET ALGORITHM **
С	** **
С	** USAGE: **
С	** **
С	** THE SECOND PART OF THE ALGORITHM ADVANCES VELOCITIES FROM **
С	** T + DT/2 TO T + DT. THIS ASSUMES THAT FORCES HAVE BEEN **
С	** COMPUTED IN THE FORCE ROUTINE AND STORED IN FX, FY, FZ. **
С	***************************************
	INTEGER N
	PARAMETER ( $N = 108$ )
	REAL DT, M, K
	REAL RX(N), RY(N), RZ(N)
	$\begin{array}{ccc} \text{REAL} & \text{VX}(\text{N}), \text{VY}(\text{N}), \text{VZ}(\text{N}) \\ \end{array}$
	REAL $FX(N)$ , $FY(N)$ , $FZ(N)$
	REAL DI2
С	***************************************
	DT2 = DT / 2.0
	K = 0.0
	DO 200 T = 1. N
!	Advances velocities from $(t + delta t/2)$ to $(t + delta t)$
	VX(I) = VX(I) + DT2 * FX(I) / M
	VY(I) = VY(I) + DT2 * FY(I) / M
	VZ(I) = VZ(I) + DT2 * FZ(I) / M
!	Compute the kinetic energy
	K = K + VX(I) ** 2 + VY(I) ** 2 + VZ(I) ** 2
	K = K + VX(I) ** 2 + VY(I) ** 2 + VZ(I) ** 2
200	K = K + VX(I) ** 2 + VY(I) ** 2 + VZ(I) ** 2 ENDDO
200	K = K + VX(I) ** 2 + VY(I) ** 2 + VZ(I) ** 2 ENDDO $K = 0.5 * M * K$
200	ENDDO K = 0.5 * M * K
200	ENDDO K = K + VX(I) ** 2 + VY(I) ** 2 + VZ(I) ** 2 ENDDO K = 0.5 * M * K RETURN

### Is the code working?: First check: the conservation laws are properly obeyed

The energy should be "constant"

In fact, small changes in energy will occur. For simple Lennard-Jones system, fluctuations of 1 part in 10<sup>4</sup> are generally considered to be acceptable

Energy fluctuations might be reduced by decreasing the time step

Suggestion to check accuracy:

Several short runs should be undertaken, each starting from the same initial configuration and covering the same total time  $t_{run}$ 

Each run should employ a different time step  $\delta t$  (different number of steps  $au_{
m run}=t_{
m run}/\delta t$  )

The root mean square fluctuations for each run should be calculated

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If the program is functioning correctly, the Verlet algorithm should give RMS fluctuations that are accurately proportional to  $\delta t^2$